

# Reme Environmental Consultants



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## Guidelines for Onsite Effluent Management Systems

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### 1.0 Summary of Problems with " Onsite Effluent Management for Single Households"

This document is "compleat" with a range of errors which make it unusable by either the professional person using this as a "Guideline" or the Council staffer, who is trying to use the "Guidelines" to assist people who are applying for Development Applications or even trying to put in a small "weekender".

### 2.0 Major Problems with the Guidelines

The guidelines revolve around the correctness of Table 6 on page 68, which is filled with errors that even a first year University student would be able to perceive. These are from the most obvious errors to extremely obscure.

In most cases, there is no basis for the items, which appear to be a "single" unit or a unit that has been "invented" for the exercise. Even when a unit "exists", the application is incorrect.

In each case, there is no reference to the text as to an explanation of the soil feature or to a reasonable reference source.

#### 2.1 Examples

##### 2.1.1 Modified Emmerson Aggregate Test

Incorrect - due to Class 1 being the most severe limitation, whereas it is shown as minor.

##### 2.1.2 Phosphorus sorption

Should be shown as kg/tonne (or mg/kg) of soil as all soils have different specific gravity's. All soils have the ability to fix P to some degree and this should be measured as routine. Using hectares, when the areas used are in square metres, just further adds to confusion.

##### 2.1.3 Cation Exchange

This section is completely misleading, as few Australian soils would be > 15, with the majority of soils being between 5 and 10 and there is no allowance for correction or changes in management systems of CEC. Further, the depths for measurement are inappropriate.

#### **2.1.4 Sodicity and Exchangeable Sodium percentage(ESP)**

The use of sodicity on its own would be appropriate, but without any allowance for correction and the mis-defining of ESP as the predominant category is not valid. The use of ESP numbers in this manner is not clear.

#### **2.1.5 Electrical Conductivity**

The units used are inappropriate.

#### **2.1.6 $pH_{CA}$**

The units used are inappropriate. The International standard is  $pH_w$  and the levels used are mis-leading.

#### **2.1.7 Bulk Density**

The ranges used are inappropriate and incorrect.

#### **2.1.8 Coarse Fragments**

There is no explicit method or rationale for these numbers.

#### **2.1.9 Soil Permeability Category**

This is an inappropriate method for this type of assessment and only causes confusion.

#### **2.1.10 Depth to Watertable**

There is no technical basis for these values. In fact a very permeable soil with over 1 metre to the water table would indeed be a problem !!!!

#### **2.1.11 Depth to bedrock**

Mixed with 2.1.12 and can be amended by the use of extra soil or larger areas.

#### **2.1.12 Depth to Hardpan**

See 2.1.11

### **3.0 General Comments**

3.1 The water balance model only uses a 5 mm/week percolation (permeability). This rate allows virtually no deep infiltration of the soil into the subsurface watertable.

3.2 A more realistic rate is required for this permeability. A rate of 25 mm/week has been adopted. This level was chosen after experimenting with the model. At this rate of percolation acceptable levels of wet weather storage was achievable. This also includes the different rainfall data to that recommended in the guidelines.

- 3.3 It was preferred that the 7th Decile rainfall data and the median evaporation data would provide a conservative estimate of wet weather storage requirements and reduce the probability of system failure due to soil saturation.
- 3.4 With the lower permeability soils would become saturated during wet months and losses due to evaporation would be lower. Assuming that there is little runoff or subsurface flow, then a much higher rate of percolation would occur simply because of the greater water potential near the soil surface, due to gravity and the lower pressure deeper in the soil.
- 3.5 Since there are no exact answers and all modelling achieves is an estimate, our methods have been designed so as to err on the side of caution.
- 3.6 The soil permeability category are inadequate for determining the limitations of the soil in regard to waterlogging, percolation and runoff.
- 3.7 The infiltration rate test is used to measure the capillarity of the soil. High capillarity allows vertical movement in the soil of water at much faster rates. Low capillarity will allow slow movement of water which will result in surface runoff or waterlogging.
- 3.8 Soil texture and structure do not give an indication of factors affecting water movement (capillarity). More important are pore space, pore size and water holding capacity which are determined by the infiltration test.
- 3.9 The percentage of coarse fragments in the soil will affect the rate of the infiltration test and is not necessary. Infiltration is greater affected by % coarse fragments with regards to limitations than would be determined from table 6
- 3.10 Bulk density has been incorrectly stated as per Table 6

#### **4.0 Basis for Comments**

We have been undertaking assessments for these types of applications for over 10 years and with little basic information that has been available for the local Municipal officer to use to assist in any "over seeing" role.

This is well shown with the errors in AS1547, which are large. These have been brought to the attention of Standards Australia, but with no response to any Faxes or letters over a 5 year period. The errors in AS1547, just in one equation are over a factor of 1440 times in just one equation.

#### **5.0 Conclusion**

The "guidelines" should be immediately withdrawn and a professional panel be used to correct errors, with all Municipal Councils advised of the errors. The professional panel must include practising soil scientists, with extensive practical and industry experience.

Signed: ..... R.W Cumming 31/10/98